

Verification Report for

Project : Wastewater Treatment and Biogas Recovery Project, SDDPL, Baramati, Maharashtra, India.

UCR Project ID : 421

Name of Verifier	SQAC Certification Pvt. Ltd.
Date of Issue	April 10, 2024
Project Proponent /	Schreiber Dynamix Dairies Private Ltd. (SDDPL),
Owner	Baramati, Maharashtra, India.
Work carried by	Mr. Santosh Nair & Ms. Sheetal Wader
Work reviewed by	Mr. Praful Shinganapurkar

Summary:

SQAC Certification Pvt. Ltd. has conducted verification of the "Wastewater Treatment and Biogas Recovery Project" at SDDPL in Baramati, Maharashtra, India. This project aims to install anaerobic digesters for the primary treatment of wastewater, specifically focusing on Mother Liquor, and subsequently harnessing methane-rich biogas produced during the process. The biogas recovered is utilized in retrofitted boilers, thereby replacing an equivalent amount of Furnace Oil (FO). This initiative contributes to the reduction of carbon dioxide (CO₂) emissions by minimizing the necessity for FO combustion in the boilers, thus mitigating environmental impact.

The project activity meets the following UN SDG's:



Verification for the period: 01/01/2014 to 31/12/2023 (10 Years, 00 Months)

Accredited by 5 Jupiter House, Callera Park, Aldermaston, Reading Berkshire RG7 8NN, United Kingdom (UK).



Email: info@sqac.in Tel: 7219716786 / 87



The GHG emission reductions were calculated on the basis of UCR Protocol Standard, CDM UNFCCC Methodology, AMS III. H: Methodology for methane recovery in wastewater treatment. version 19 and AMS-I.C: Methodology for Thermal energy production with or without electricity version 22. The verification was done onsite by way of interviews, onsite document verification and submission of documents for verification.

SQAC is able to certify that the emission reductions from the project Wastewater Treatment and Biogas Recovery Project, SDDPL, Baramati, Maharashtra, India, (UCR ID – 421) for the period **01/01/2014 to 31/12/2023** amounts to **1,23,792 tCO₂ (1,23,792 CoUs)**

Detailed Verification Report:

Purpose:

Schreiber Dynamix Dairies Pvt. Ltd., (SDDPL), also called as Project Proponent (PP) a fully integrated dairy industry is located at Baramati in the state of Maharashtra, India.

The PP has full ownership of the project activity. This project is an operational activity with continuous reduction of GHGs, currently being applied under "Universal Carbon Registry" (UCR).

In June 2015, under Section 18 of the Companies Act 2013, Schreiber Dynamix Dairy Limited was changed into Schreiber Dynamix Dairy Private Limited (SDDPL).

The daily processing capacity of plant is 800,000 - 1,600,000 liters of milk/day which is sourced from surrounding districts. It produces various dairy products through superior technology and process. The products include cheese, butter, ghee, casein, skimmed milk powder, dairy whitener, lactose, whey protein concentrate, whey powder and juices (milk and fruit) in aseptic packing.

While manufacturing of above products the wastewater is generated in two streams:

- Wastewater generated through processing of milk, yogurt, and other dairy products
- Wastewater generated from production of dairy products such as cheese and casein.

Project Activity scenario:

- i. Wastewater generated through processing of milk, yogurt and other dairy products will continue to be treated in the existing 4,500 m3/day Wastewater Treatment Plant (WWTP). The biogas generated from anaerobic treatment is captured and is used to fire in the retrofitted boilers with dual fuel burner.
- ii. The wastewater generated from production of dairy products such as cheese and casein. A by product called 'whey' is generated during manufacturing of these products. During Lactose



recovery from whey, Mother Liquor (De-Lactose Permeate (DLP)) is generated. Mother liquor has a typical characteristic of 95.62% organic matter having organic load, COD in the range of 250,000 mg/liter to 390,000 mg/liter. This mother liquor is treated in a specially designed RCC constructed anaerobic treatment plant - Mother Liquor Treatment Plant (MLTP) with methane recovery.

- iii. Post recovery of methane, additional treatment on mother liquor is needed due to its high organic load. Therefore, it is further treated in the existing 4,500 m³/day WWTP. Outlets from MLTP get mixed with other stream of wastewater at equalization tank and treated in 4,500 m3/day WWTP.
- iv. The biogas generated from four anaerobic digesters of 4,500 m³/day WWTP, two anaerobic digesters of 45 m³/day MLTP will be captured and fired in the existing retrofitted boiler RFB 60, SM140.1 & SM140.2 (SM140.1 and SM140.2 which are stand-by boilers for RFB 60. The generated biogas is used exclusively in RFB-60 boiler.)

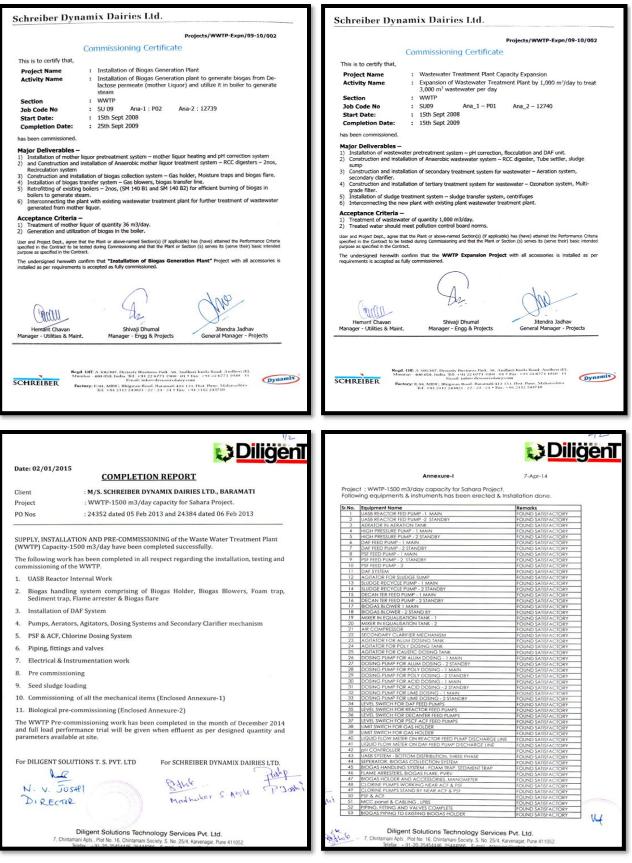
The UCR project activity involves greenhouse gas emissions reduction through two methods:

- 1. Firstly, by directing the flow of Mother Liquor into closed anaerobic digesters, which prevents the release of methane (CH₄) into the atmosphere; and
- 2. Secondly, by utilizing biogas generated from a 45 m³/day Mother Liquor Treatment Plant (MLTP) and an existing 4,500 m³/day Wastewater Treatment Plant (WWTP) in retrofitted boilers, replacing an equivalent quantity of Furnace Oil (FO) or Low Sulphur Heavy Stock (LSHS). This substitution reduces carbon dioxide (CO₂) emissions by decreasing the amount of FO burned in the boilers, thus contributing to overall emissions reduction.

The UCR project activity qualifies under the environmental additional positive list of pre-approved project types under the UCR carbon incentive model for issuance of voluntary carbon credits.

UCR Monitoring Period Number	01
Start Date (DD/MM/YYYY)	01/01/2014
End Date (DD/MM/YYYY)	31/12/2023
Total Emission Reductions over the monitoring period (CoUs)	1,23,792 tCO ₂



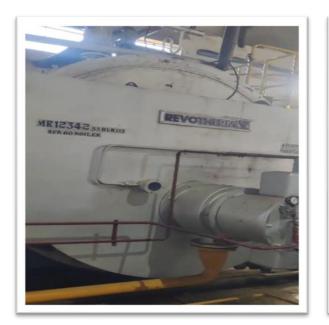




Pollution Board Renewal of Existing Consent to Operate - 08/07/2020.

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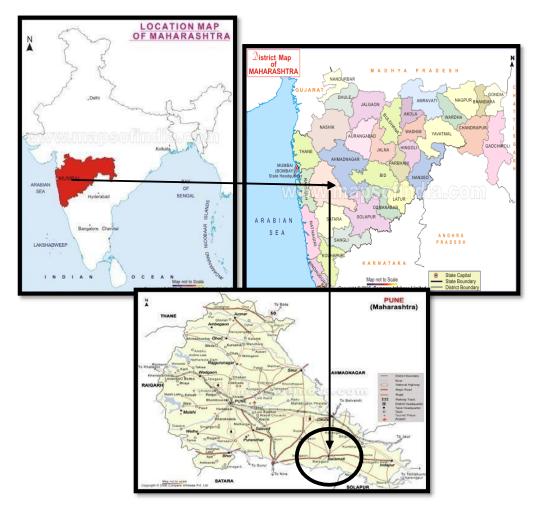




Location of project activity:

Country	: India
District	: Pune
Taluka	: Baramati
State	: Maharashtra
Pincode	: 413133
Latitude	: 18º11'24.16"N
Longitude	: 74 ⁰ 37' 06.04"E





Source: Google map



Biogas generation site



Scope:

The scope covers verification of emission reductions from the project - Wastewater Treatment and Biogas Recovery Project, SDDPL, Baramati, Maharashtra, India, (UCR ID – 421).

Criteria:

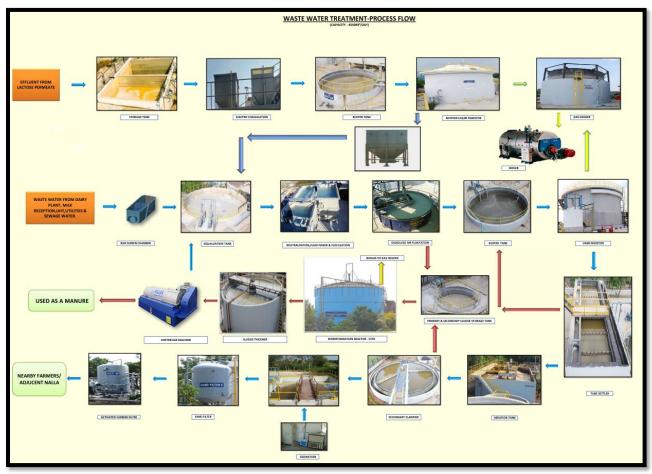
Verification criteria is as per the requirements of UCR Standard.

Description of project:

The UCR project activity involves treatment of mother liquor through following major stages:

- 1. Mother Liquor Treatment with anaerobic digesters.
- 2. Biogas Generation, Capture and Transfer to Boilers.
- 3. Utilization of biogas in boilers as a fuel for partial displacement of furnace oil.
- 4. Treatment on wastewater generated from mother liquor treatment plant

The project activity is generating steam for captive purposes using biogas from MLTP and WWTP Each of the above stages of the project activity is briefly explained below in the diagram:





United Nations Sustainable Development Goals:

The project activity is for primary treatment of wastewater (namely Mother Liquor) and subsequently recovering methane rich biogas generated during the process at Schreiber Dynamix Dairies Pvt. Ltd. And the recovered biogas will be used in retrofitted boilers replacing equivalent quantity of FO (Furnace Oil).

Thus, the renewable energy generation from project activity will result in reduction of the greenhouse gas emissions. Positive contribution of the project to the following Sustainable Development Goals:

- SDG 7: Affordable and Clean Energy
- SDG 9: Industry, Innovation, and Infrastructure
- SDG12: Responsible Consumption and Production
- SDG13: Climate Action
- SDG15: Life on Land

Technical details of the project activity

The waste water treatment system consists of the following equipment: Characteristics of the equipment installed:

Design basis for 45m³/day mother liquor:

The design basis considered to size the various units for Mother Liquor treatment is as follows:

Characteristics	Mother Liquor
Total flow	45 m³/day
COD	390,000 mg/liter
BOD	220,000 mg/liter
TSS	5 % (w/v)
рН	3 – 5.5

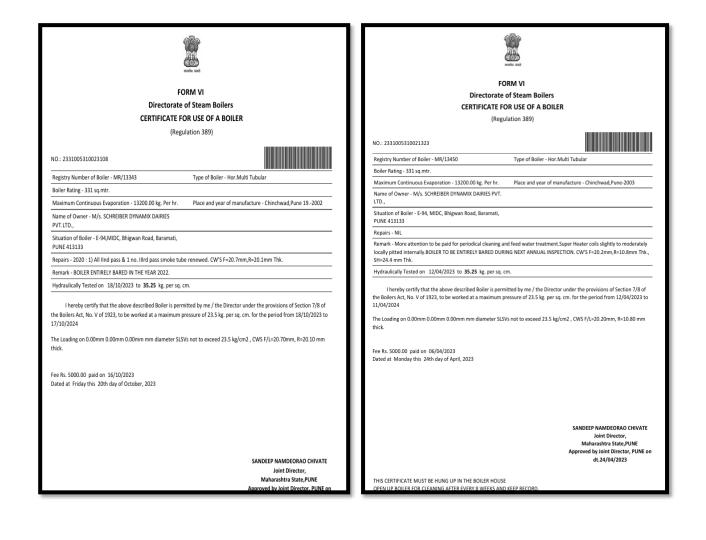
Technical specification of Stand-by boilers: (MR13343, MR13450)

Appliance	: Steam boiler
Туре	: 3 pass, conventional, smoke tube type
Make	: Thermax Ltd.
Model	: SM 140 B
Sr. No.	: MR13343, MR13450
Steam generation capacity	: 13200 kg/hr (F&A 100ºC)
Designed pressure	: 23.5 kg/cm ² g
Design temperature	: 250.0°C
Combustion air temperature	: Ambient
Present thermal efficiency considered	: 89% ⁶ @ NCV with economizer



Technical specification of boilers: (MR12342)

Appliance	: Steam boiler
Туре	: 1 pass, conventional, smoke tube type
Make	: Thermax Ltd.
Model	: RFB60
Sr. No.	: MR 12342
Steam generation capacity	: 6000 kg/hr (F&A 100ºC)
Designed pressure	: 17.5 kg/cm ² g
Design temperature	: 207.0°C
Combustion air temperature	: Ambient
Present thermal efficiency considered	: 89% ⁶ @ NCV with economizer





	THERMAX LIMITED D-13, MIDC INDUSTRIAL AREA, R. D. AGA ROAD, CHINCHWAD, PUNE 411 019, INDIA □ TEL : (020) 27475941 (5 LINES) □ FAX : (D) (020) 27477060, 27472049 □ Website : www.thermaxindia.com □ IT PAN - AAACT3910D
सर्वव्य व्यव्य	
FORM VI	
Directorate of Steam Boilers	Cooling & Heating Division THERMAX
CERTIFICATE FOR USE OF A BOILER	
(Regulation 389)	
NO.: 2431005310024187	Date of Report: 31/01/2014
Registry Number of Boiler - MR/12342 Type of Boiler - Flue Tube Shell Type	Customer: M/S Schreiber Dynamix Dairy Ltd. Baramati
Boiler Rating - 100 sq.mtr.	Purpose of Visit: Commissioning of Gas Conversion unit on RFB-60 Unit.
Maximum Continuous Evaporation - 6000.00 kg, Per hr. Place and year of manufacture - Pune-1994	
Name of Owner - M/s. SCHREIBER DYNAMIX DAIRIES PVT. LTD.,	Customer Contact person: Mr. Narayan Korde, Sachin Zadbuke (Maint.) & Mr. C. Bhagat (Safety)
Situation of Boiler - E-94,MIDC, Bhigwan Road,Baramati, PUNE 413133	Thermax Engineer: Mr. Amit Patil, Mr. Vijay Khawale, Mr. Varun Patil
Repairs - 1997: One tube renewed.2002: Connection for level transmitter and 2 nos. surface blow down with dummy provided.33 nos. of tubes renewed.2008: 3 nos. tubes renewed.2015 : One smoke tube renewed.	Date of Visit: 29/01/2014 to 31/01/2014
Remark - More attention to be paid for periodical cleaning and feed water treatment. CW'S F=18.68mm,R=17.8mm Thk.	
Hydraulically Tested on 03/01/2024 to 26.50 kg. per sq. cm.	Observations and activities:
I hereby certify that the above described Boiler is permitted by me / the Director under the provisions of Section 7/8 of the Boilers Act, No. V of 1923, to be worked at a maximum pressure of 17.5 kg, per sq. cm. for the period from 03/01/2024 to 02/01/2025 The Loading on 0.00mm 0.00mm 0.00mm mm diameter SLSVs not to exceed 17.5 kg/cm2 , CWS F/L=18.68mm, R=17.80 mm thick. Fee Rs. 4000.00 paid on 01/01/2024 Dated at Tuesday this 9th day of January, 2024	 Burner gun were received at site after repair, same was installed on unit and trial taken for firing on oil (100%) modulation from low to high. Burner air setting kept suitable for single fuel either biogas (Fix 30% opening suitable for current flow of 150 Nm3/hour avg. gas) or FO (100 % modulation). Unit load trail taken with available biogas flow for around 12 hrs on 29/01/2014 & 30/01/2014. Found maximum load were carried by unit is around 2.5 TPH As per operations requirement the gas low pressure switch. It was observed that after each stoppages or tripping incoming gas pressure increasing more than rated (As per P&I - 2000 mmVC), hence to complete commissioning trials Gas pressure High switch is bypassed and commissioning trials completed. After fine tuning below parameters noted down for respective fuels.
SANDEEP NAMDEORAO CHIVATE Joint Director, Maharashtra State,PUNE Approved by Joint Director, PUNE on	Fuel % Burner Burner Stack Return Temp. O2 % CO ppm
dt.09/01/2024	opening Pressure(Pressure((degC) Kg/Cm2) Kg/Cm2)
THIS CERTIFICATE MUST BE HUNG UP IN THE BOILER HOUSE OPEN UP BOILER FOR CLEANING AFTER EVERY 8 WEEKS AND KEEP RECORD.	Bio Gas 30 400MMWC NA 200 8 50
	FO 40 15 6 226 5. 28

Level of Assurance:

The verification report is based on onsite audit, information collected through interviews, supporting documents provided during the verification, Project Concept Note (PCN), Monitoring Report (MR) submitted to SQAC. The verification opinion is assured provided the credibility of all the above.

Review of the following documentation was done by SQAC Verifier, Mr. Santosh Nair and Ms. Sheetal Wader, who is experienced in such projects.

Documentation Verified:

- Project Concept Note (PCN)
- Monitoring Report (MR)
- Month wise Quantity of
 - Biogas combusted in the project plant.
 - o Steam generation



- Electricity consumption
- Furnace oil consumption
- Environmental Clearance
- Commissioning Certificate
- Boiler Certificates
- Shift log books
- Calibration Certificates
- COD Reports
- Waste water generation
- Mother liquor generation
- Data provided upon request of all the documents of the related project.
- JMR's
- Invoices

Sampling:

Not applicable

Person interviewed:

Sr. No.	Auditee Name	Designation	Company
1	Mr. Jitendra Jadhav	Operations Director	Schreiber Dynamix Dairies Pvt. Ltd., India.
2	Mr. Hanumant Jagtap	Plant Manager	Schreiber Dynamix Dairies Pvt. Ltd., India.
3	Mr. Hemant Chavan	Team Leader - Utilities and Maintenance	Schreiber Dynamix Dairies Pvt. Ltd., India
4	Mr. Shivaji Dhumal	Team Leader - Engineering Projects	Schreiber Dynamix Dairies Pvt. Ltd., India.
5	Mr. Ankush Darekar	Team Leader – Elec., Instr. & control	Schreiber Dynamix Dairies Pvt. Ltd., India.
6	Mr. Mansing Mande	Team Advisor - Water, WWTP & Environment	Schreiber Dynamix Dairies Pvt. Ltd., India.
7	Mr. Satish Bhosale	Senior Associate - Boiler	Schreiber Dynamix Dairies Pvt. Ltd., India
8	Mr. Balasaheb Kokare	Senior Associate - Utility Maintenance	Schreiber Dynamix Dairies Pvt. Ltd., India.
9	Mr. Ajay Bandal	Senior Associate - Utility Maintenance	Schreiber Dynamix Dairies Pvt. Ltd., India
10	Mr. Prathamesh Godase	Project Manager - Carbon Credits	Climekare Sustainability Pvt. Ltd.



Ba	ramati, P	une, Satara			M : 937 I2011@rediffmai	I, Ashoknagar, Bar 0475047 / 8975689 I.com / Rajc		mail.com	11-	Baramati, P	Pune, Satara		Rajcontro		0475047 / 8975689 il.com / Rajc		mail.com	
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	-	-		TAL MULTIMETER RC-04		580		2245417	28/03/2024			
		2				504		2240417		-	Sr. Description	
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8	-	-	TY: < 70 % R									
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							1				Accuracy ± (0.06 % OF RDG + 4 DIG.)	; 1

<u>(</u>	SBQUA Colloration I Validat Head Office : Flat No. Pune - 411 043. Mahar	on I Testing & Me 13. Ganesh Darshar	asurement I Si	ales & Services	C 982232	0146
Certificate No.	2246417	<u>Certificate of C</u>	Calibration			Page 1 of 12
Client Raj Control's Flat No.01 , Gajra Appt. , Asho Bhigwan Road , Baramati.	əknagar,		Date of Recei Physical Cont Customer Ser UUC Calibrat	dition rvice Request	29.03.2023 Satisfactory P.O. In Lab.	C0.2360
Cal. Date : 29.03.2023		Cal. Freq. :	12 months	Rec. Due Dat	e: 28.03.202	4
		Description	of UUC			
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	160	159.98	-0.020	0.136	0.28	ок
	240	239.98	-0.020	0.184	0.28	ок
	320	319.97	-0.030	0.232	0.28	ок
	390	389.96	-0.040	0.274	0.28	ок
	Masterland	UUC Reading		Permissible	Uncertainty in	Remark
	Master Instrument Reading In V DC	in V DC	Error	Error	± %	
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Frequ		Mother Liquor	1		Digester I		Pressure	Temp.	Generation NM3/hr. FIQ-56MLD0
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		M ³ /Hr. FIQ32T07	MMWC		30	30			30
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12.00 AM	A	0.7	-	-	31	3)	-	-	30
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Certificate No.	\$ 2246432	Certificate of C	Calibration		Page 1 of
Client Raj Control's Flat No.01 , Gajra Appt. , Asho Bhigwan Road , Baramati.	knagar,		Date of Receipt Physical Conditio Customer Service UUC Calibrated	Request P.O. at On site	06-2342
- al. Date : 29.03.2023		Cal. Freq. :		Rec. Due Date : 28.0	3.2024
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Sr. Description 1 5 & % Dig.Multimeter	Sr. / ID No. 118319		fied By	Certificate No.	Validity
2 Universal Calibrator.	DCB-03		Gandhinagar. Gandhinagar.	E/G0223/0121/22-23 E/G1023/0064/2022	27.02.2025
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Accuracy ± 1 % F.S.D.	-199.00	-199.00	0.000	0.32	ок
	-150.01	-150.00	0.005	0.32	ок
	-100.01	-100.00	0.005	0.32	ок
	-50.01	-50.00	0.005	0.32	ок
	0.00	0.00	0.000	0.32	ок
Range 0 to 199.99 mV DC Least Count 0.01 mV DC	Master Instrument Reading in mV DC	UUC Readin in mV DC	ng Error in %	Uncerta ± %	
Accuracy ± 1 % F.S.D.	0.00	0.00	0.000	0.32	OK







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Applied methodologies and standardized baselines:

UCR Protocol Standard

SECTORAL SCOPE	- 13 Waste handling and disposal.
ΤΥΡΕ Ι	- III - Other project activities.
CATEGORY	- AMS-III.H. Methane Recovery in Wastewater Treatment, version 19.
SECTORAL SCOPE	- 01 Energy Industries (Renewable / Non-renewal Sources)
ΤΥΡΕ Ι	- Renewable Energy Projects
CATEGORY	 AMS-I.C. Thermal energy production with / without electricity, version 22.

The project activity involves mother liquor treatment in anaerobic digesters that otherwise would continue to be treated in anaerobic deep lagoons without any biogas recovery. Generated biogas in the project activity is used in the boiler thereby replacing corresponding quantity of FO.



Hence, simplified baseline for the project activity is, continued treatment of Mother Liquor in anaerobic deep lagoons without biogas recovery and consumption of equivalent quantity of FO that otherwise would have been consumed in the boiler to generate corresponding quantity of steam.

Application of methodologies and standardized baselines

For AMS III.H. Version 19

Applicability Clause	Applicability Criteria	Project activity	Accepted?
2.1 - 2	This methodology comprises measures that recover biogas frombiogenic organic matter in wastewater by means of one, or a combination, of the following options:	The methodology comprises measures that recover biogas from biogenic organic matter in the waste water (Mother Liquor composing of Carbohydrates, proteins & fat) by means of applicability criteria option (f).	Yes
2.1 –2 a)	wastewater or sludge treatment systems with anaerobic systems	This criterion is not applicable since the project activity involves replacement of existing anaerobic system.	Yes
2.1 – 2 b)	treatment system with biogas recovery and combustion to a	This criterion is not applicable since the project activity does not involve installation of anaerobic sludge treatment system.	Yes
2.1 – 2 c)	Introduction of biogas recovery andcombustion to a sludge treatment system.	This criterion is not applicable since the project activity does not involve introduction of biogas recovery and combustion to an existing sludge treatment system.	Yes
2.1 – 2 d)	Introduction of biogas recovery and combustion to an anaerobic wastewater treatment system such asanaerobic reactor, lagoon, septic tank or an on site industrial plant.	This criterion is not applicable since theproject activity does not involve introduction of biogas recovery to anexisting treatment system i. e. anaerobic lagoon.	Yes



2.1 – 2 e)	Introduction of anaerobic wastewater treatment with biogasrecovery and combustion, with orwithout anaerobic sludge treatment,to an untreated wastewater stream.	This criterion is not applicable since the project activity involves installation of Up flow Anaerobic Sludge Blanket digesters with methane recovery and combustion to a waste water stream which was previously treated in an existing anaerobic wastewater treatment system i.e., anaerobic lagoon.	Yes
2.1 – 2 f)	Introduction of a sequential stage of wastewater treatment with biogas recovery and combustion, with or without sludge treatment, to an anaerobic wastewater treatment system without biogas recovery (e.g.introduction of treatment in an anaerobic reactor with biogas recovery as a sequential treatment step for the wastewater that is presently being treated in an anaerobic lagoon without methane recovery).	This criterion is applicable since the project activity involves installation of Up flow Anaerobic Sludge Blanket digesters with methane recovery and combustion followed by further treatment in aerobic as well as	Yes
2.2 – 3	In cases where baseline system is anaerobic lagoon the methodology isapplicable if;		Yes
2.2 – 3 a)	(a) The lagoons are ponds with a depth greater than two meters, without aeration. The value for depth is obtained from engineering design documents, or through directmeasurement, or by dividing the surface area by the total volume. If the lagoon filling level varies seasonally, the average of the highest and lowest levels may be taken	The anaerobic lagoons are ponds with a depth greater than two meters, without aeration	Yes
2.2 – 3 b)	(b) Ambient temperature above 15 ^[2] C, at least during part of the year, on a monthly average basis	Ambient temperature of the Project site isabove 15Con a monthly average basis	Yes



2.2 – 3 c)	(c) The minimum interval betweentwo consecutive sludge removal events shall be 30 days	The minimum interval between two consecutive sludge removal events is 30days	Yes
2.2 – 4	The recovered biogas from the above measures may also be utilized for the following applications instead of combustion/flaring.		Yes
2.2 – 4 a)		This criterion is applicable since the project activity involves utilization of recovered biogas for thermal energy generation directly in boilers for steam generation.	Yes
2.2 – 4 b)	energy generation after bottling of upgraded biogas, in this case	This criterion is not applicable since the recovered biogas is utilized for thermal energy generation directly without bottling	Yes
2.2 – 4 c)	 additional guidance provided in theappendix shall be followed: (i) Upgrading and injection of biogas into a natural gas distributiongrid with no significant transmission constraints; (ii) Upgrading and transportation ofbiogas via a dedicated piped network to a group of end users; or (iii) Upgrading and 	This criterion is not applicable since the recovered biogas is utilized for thermal energy generation directly without upgrading and distribution. This criterion is not applicable since there is no upgrading and injection of biogas into a natural gas distribution grid. This criterion is not applicable since there is no up gradation and transportation of biogas via a dedicated piped network to a group of end users. This criterion is not applicable since there is no upgrading and transportation of biogas (e.g. by trucks) to distribution points for end users.	Yes
2.2 – 4 d)	Hydrogen production	This criterion is not applicable since there is no hydrogen production from the recovered biogas.	Yes



2.2 – 4 e)	Use as fuel in transportation applications after upgrading	This criterion is not applicable since biogas is not used as fuel in transportation applications after upgrading	Yes
2.2 – 5)	If the recovered biogas is used for project activities covered under paragraph 4(a), that component ofthe project activity can use a corresponding methodology underType I.	The recovered biogas is used for thermal (steam) energy generation in project activities covered under paragraph 4 (a) and hence the project activity can use a corresponding methodology under Type I and the methodology AMS I.C. is used	Yes
2.2 – 6)	For project activities covered under paragraph 4 (b), if bottles with upgraded biogas are sold outside the project boundary, the end-use of the biogas shall be ensured via a contract between the bottled biogas vendor andthe end-user. No emission reductions may be claimed from the displacementof fuels from the end use of bottled biogas in such situations. If however the end use of the bottled biogas is included in the project boundary and is monitored during the crediting period CO2 emissions avoided by the displacement of fossil fuel can be claimed under the corresponding Typel methodology, e.g. AMS-I.C "Thermal energy production with or without electricity".		Yes
2.2 – 7)	For project activities covered under paragraph 4 (c) (i), emission reductions from the displacement of the use of natural gas are eligible under this methodology, provided the geographical extent of the natural gasdistribution grid is within the host country boundaries.	This criterion is not applicable since project activity is not covered under paragraph 4 (c) (i).	Yes



2.2 – 8)	For project activities covered under paragraph 4(c)(ii), emission reductions for the displacement of theuse of fuels can be claimed following the provision in the corresponding Type I methodology, e.g. AMS-I.C.	This criterion is not applicable since project activity is not covered under paragraph 4 (c) (ii).	Yes
2.2 – 9)	In particular, for the case of paragraph4(b) and (c)(iii), the physical leakage during storage and transportation of upgraded biogas, as well as the emissions from fossil fuel consumed by vehicles for transporting biogas shall be considered. Relevant procedures in paragraph 18 of the appendix of "AMS-III.H.: Methane recovery in wastewater treatment" shall be followed in this regard	This criterion is not applicable since projectactivity is not covered under paragraph 4 (b) and (c) (iii).	Yes
2.2 – 10)	For project activities covered under paragraph 4(b) and (c), this methodology is applicable if the upgraded methane content of the biogas is in accordance with relevant national regulations (where these exist) or, in the absence of national regulations, a minimum of 96 per cent(by volume)	This criterion is not applicable since project activity is not covered under paragraph 4 (b)and (c).	Yes
2.2 – 11)	If the recovered is utilized for the production of hydrogen (project activities covered under paragraph 3(d)), that component of the project activity shall use the corresponding methodology "AMS-III.O.: Hydrogen production using methane extractedfrom biogas".	This criterion is not applicable since the recovered biogas is not utilized for production of hydrogen.	Yes
2.2 – 12)	If the recovered biogas is used for project activities covered under paragraph 4(e), that component of theproject activity shall use corresponding methodology "AMS- III.AQ.: Introduction of Bio-CNG intransportation applications".	This criterion is not applicable since the recovered biogas is not used for project activities covered under paragraph 4 (e).	Yes

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2.2 – 13)	New facilities (Greenfield projects) and project activities involving a change of equipment resulting in a capacity addition of the wastewater orsludge treatment system compared to the designed capacity of the baseline treatment system are only eligible to apply this methodology if they complywith the relevant requirements in the "General guidelines for SSC CDM methodologies". In addition, the requirements for demonstrating the remaining lifetime of the equipment replaced, as described in the general guidelines shall be followed.	The project activity is not a green field project and it does not involve any change of equipment resulting in a capacity addition of the wastewater treatment system compared to the designed capacity of the baseline treatment system.	Yes
2.2 – 14)	The location of the wastewater treatment plant shall be uniquely defined as well as the source generating the wastewater shall beuniquely defined and described in the PCN.	The location of the wastewater treatment plant is defined in PCN. The sourcegenerating the wastewater is process units for manufacturing of dairy products and other products at SDDPL is defined in PCN	Yes
2.2 – 15)		The project activity will result in emission reduction of 12,000 tCO2 annually which isless than 60 kt CO2 equivalent annually	Yes

For AMS I.C. Version 22

Applicability Clause	Applicability Criteria	Project activity	Accepted?
2.2 – 3)	and tri-generation systems are included in this category.	The project activity does not involve biomass based cogeneration system and hence this criterion is not applicable.	Yes



· · ·			
2.2 – 4)	biomass cogeneration	The project activity does not involve biomass cogeneration and hence none of the activities is applicable.	Yes
2.2 – 5)	Project activities that seek to retrofitor modify an existing facility for renewable energy generation are included in this category.	retrofitting the existing facilities	Yes
2.2 – 6)	In the case of new facilities (Greenfield projects) and project activities involving capacity additions the relevant requirementsrelated to determination of baseline scenario provided in the "General guidelines for SSC CDM methodologies" for Type-II and Type-III Greenfield/capacity expansion project activities also apply.	The project activity does not involvecapacity addition.	Yes
2.2 – 7)	The total installed/rated thermalenergy generation capacity of theproject equipment is equal to or less than 45 MW thermal	The total installed/rated thermal energy generation capacity of the project equipment is 6.5 MW	Yes
2.2 – 8)	For co-fired systems, the total installed thermal energy generationcapacity of the project equipment, when using both fossil and renewable fuel, shall not exceed 45MW thermal (see paragraph 9 for the applicable limits for cogeneration project activities).	The Project activity is a co-fired system and the total installed thermal energy generation capacity of the project equipment, when using both fossil and renewable fuel is 16.56 MW thermal and does not exceed 45 MW thermal.	Yes



2.2 – 9)	The following capacity	The project activity does not	
	limits apply for biomass	involve biomass co-generation and	
	cogenerationand tri-	hence none ofthe activities is	
	5	applicable.	
	(a) If the emission		
	reductions of the project		
	activity are on account of		
	thermal and electrical		
	energy production, the total		
	installed thermal and		
	electrical energy generation		
	capacity of the project		
	equipment shall not exceed		
	45 MWthermal. For the		
	purpose of calculating the		
	capacity limit the conversion		
	factor of 1:3 shall be used		
	for converting electrical		
	energy to thermal energy		
	(i.e. for renewable energy		
	project activities,the		
	installed capacity of 15		
	MW(e)is equivalent to 45		
	MW thermal output of the		
	equipment or the plant);		Yes
	(b) If the emission		
	reductions of the project		
	activity are solely on		
	account of thermal energy		
	production (i.e. no emission		
	reductions accrue from the		
	electricity component), the		
	total installed thermal		
	energy productioncapacity		
	of the project equipment		
	shall not exceed 45 MW		
	thermal;		
	(c) If the emission		
	reductions of the project		
	activity are solely on		
	account of electrical energy		
	production (i.e. no emission		
	reductions accrue from the		
	thermalenergy component),		
	the total installed electrical		
	energy generation capacity		
	of the projectequipment		
	shall not exceed 15 MW.		



2.2 – 10)	The capacity limits specified in paragraphs 7 to 9 above apply toboth new facilities and retrofit projects. In the case of project activities that involve the addition of renewable energy unitsat an existing renewable energy facility, the total capacity of the units added by the project shall comply with capacity limits specified in the paragraphs 7 to 9, and shall be physically distinctfrom the existing units	The project activity does not involve addition of renewable energy units at existing renewable energy facility.	Yes
2.2 – 11)	If solid biomass fuel (e.g. briquette) is used, it shall be demonstrated that it has been produced using solely renewable biomass and all project or leakageemissions associated with its production shall be taken into account in the emissions reduction calculation.	The project activity does not involve solidbiomass fuel (e.g. briquette).	Y e s
2.2 – 12)			Yes
2.2 – 13)	If electricity and/or thermal energyproduced by the	The steam produced by the project activity is not delivered to a third party i.e. another facility or facilities within the project boundary.	Yes



	that ensuresthere is no double-counting of emission reductions.		
2.2 – 14)	If the project activity recovers andutilizes biogas for producing electricity and/or thermal energy and	The project activity recovers and utilizes biogas for heat production and type III component of a SSC methodology is considered i. e. AMS	
	applies this methodology on astandalone basis i.e. without usinga Type III component of a SSC methodology, any incremental emissions occurring due to the implementation of the project activity (e.g. physical leakage of the anaerobic digester, emissions due to inefficiency of the flaring), shall be taken into account either as project or leakage emissions as per relevant procedures in the tool"Emissions from	Ш.Н.	Yes
	solid waste disposal sites" and/or "Project emissions from flaring". In the event that the biomass fuel (solid/liquid/gas) is sourced from an existing CDM project, then theemissions associated with the production of the fuel shall be accounted with that project.		Yes
2.2 – 15)	If project equipment contains refrigerants, then the refrigerant used in the project case shall haveno ozone depleting potential (ODP).	The project activity does not involve refrigerants and hence not applicable.	Yes



2.2 – 16) Charcoal based biomass energy generation project activities are eligible to apply the methodology only if the charcoal is produced from renewable biomass sources, provided: (a) Charcoal is produced in kilns equipped with methane recovery and destruction facility; or (b) If charcoal is produced in kilns not equipped with a methane recovery and destruction facility, or (b) If charcoal is produced in kilns not equipped with a methane recovery and destruction facility, methane emissions from the production of charcoal shall be considered. These emissions shall be calculated as per the procedures defined in the approved methodology "AMS-III.K.: Avoidance of methane release from charcoal production by shifting from traditional open- ended methods to mechanized	_
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are generation. Yes generation. Yes methodology only if the charcoal is produced from renewable biomass sources, provided: (a) Charcoal is produced in kilns equipped with methane recovery and destruction facility; or (b) If charcoal is produced in kilns not equipped with a methane recovery and destruction facility, methane emissions from the production of charcoal shall be considered. These emissions shall be calculated as per the procedures defined in the approved methodology "AMS-III.K.: Avoidance of methane release from charcoal production by shifting from traditional open-ended methods to	
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from charcoal production by shifting from traditional open- ended methods to	
shifting from traditional open- ended methods to	
open- ended methods to	
ended methods to	
imechanized	
charcoaling process".	
Alternatively, conservative	
emission factor values from	
peer	
reviewed literature or from a	
registered CDM project	
activity	
can be used, provided that it	
can be	
demonstrated that the	
parameters	
from these are comparable	
e.g.	
source of biomass,	
characteristics	
of biomass such as moisture,	
carbon content, type of kiln,	
operating conditions such as	
ambient temperature.	



2.2 – 17)	In the case the project	The	project	activity	does not	
	activities utilizes biomass, the	utilize	e biomass			
	"TOOL16: Project and leakage					
	emissions frombiomass" shall					
	be applied to determine the					Yes
	relevant project emissions					
	from the cultivation of					
	biomass and the utilization of					
	biomass or biomass residues.					

Applicability of double counting emission reductions

The project activity has been registered as a CDM project activity (registration date of the project activity under CDM mechanism is 04/09/2012) in the past as follows:

UNFCCC CDM Title	Waste water tr	eatment and biogas recovery			
	project				
CDM ID	2503				
Host Parties	Schreiber Dynamix Dairies Ltd.				
Sectoral Scopes	1: Energy inc	lustries (renewable - / non-			
	renewable sources)				
	13: Waste handl	ing and disposal			
Methodology	AMS-III.H. ver. 19 - Methane recovery in				
	wastewater treatment				
	AMS-I.C. ver. 22 - Thermal energy production				
	with or without	electricity			
Other Details	CDM	04 Sep 12 (Date of registration			
	Registration	action 15 Nov 12)			
	Date				
	Crediting	04 Sep 12 - 03 Sep 22 (Fixed)			
	Period				
Prior Issuance of CDM credits	Nil				

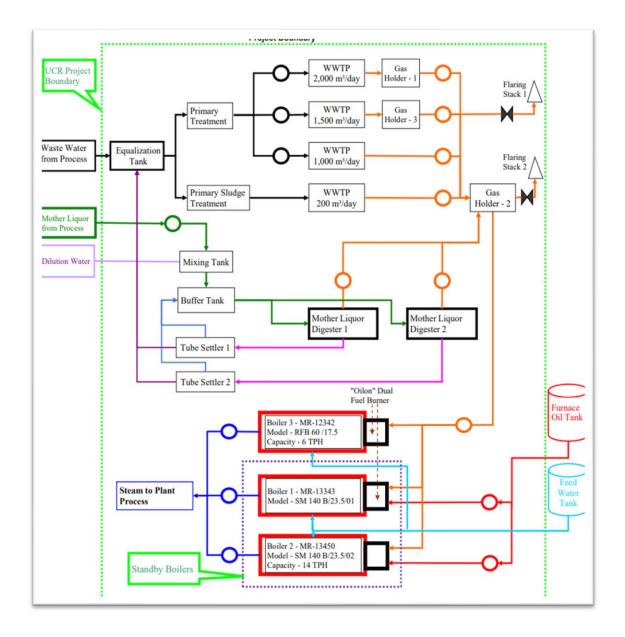
The project activity was registered under CDM under ID 2503 on 04 Sep 12 for the 04 Sep 12 - 03 Sep 22, however no CER's have been issued for the same. The project activity is now seeking CoUs under the UCR CoU Standard/Program for the period 01/01/2014 to 31/12/2023 and hence there is no double counting issue of carbon credits for the said vintageperiod. Additionally, the same has been stated in the undertaking provided in the Double Counting Avoidance Assurance Document (DAA) by SDDPL dated 09.04.2024.



Project boundary, sources and greenhouse gases (GHGs)

The project boundary includes the physical, geographical site(s) of:

- a) where the wastewater and sludge treatment takes place, in the baseline and project situations. It covers all facilities affected by the project activity including sites where processing, transportation and application or disposal of waste products as well as biogas takes place.;
- b) All power plants generating power and/or heat located at the project site, whether fired with biomass, fossil fuels or a combination of both;





The following table summarizes the source and type of emissions associated with the project activity:

	Source	Gas	Included	Justification /Explanation
	Combustion of	CO ₂	Included	Emissions due to Furnace oil combustion for the steam generation.
	FurnaceOil (FO) for	CH ₄	Excluded	Excluded for simplification
line	steam generation	N ₂ O	Excluded	Excluded for simplification
Baseline	Mother Liquor	CO ₂	Excluded	Excluded for simplification
	treatmentin Anaerobic	CH ₄	Included	Emissions due to mother liquor treatment in anaerobic lagoons
	Lagoon	N ₂ O	Excluded	Excluded for simplification
		CO ₂	Excluded	Excluded for simplification
	Existing Waste	CH ₄	Included	Emissions due to Waste water treatment.
	watertreatment System	N ₂ O	Excluded	Excluded for simplification
Project activity	Combustion of Furnace	CO ₂	Included	Emissions due to Furnace oil combustion for the steam generation.
Pro acti	Oil(FO) for steam generation	CH ₄	Excluded	Excluded for simplification
		N ₂ O	Excluded	Excluded for simplification
	Electricity consumption	CO ₂	Included	Emission due to electricity consumption in the project activity
	Liectricity consumption	CH ₄	Excluded	Excluded for simplification
		N ₂ O	Excluded	Excluded for simplification
		CO ₂	Excluded	Excluded for simplification
	45 m ³ /day Mother	CH ₄	Included	Emissions due to mother liquor treatment
	Liquortreatment system	N ₂ O	Excluded	Excluded for simplification
		CO ₂	Excluded	Excluded for simplification
	4,500 m³/day Wastewater	CH ₄	Included	Emissions due to affected part of waste water treatment
	treatment systems	N ₂ O	Excluded	Excluded for simplification
		CO ₂	Excluded	Excluded for simplification
	Biogas flaring system	CH ₄	Included	Emissions due to inefficiency in the flaring system
		N ₂ O	Excluded	Excluded for simplification



Baseline Emissions (BE_y)

Baseline emissions as per AMS III. H.

 $BE_{y} = \left\{ BE_{power,y} + BE_{ww,treatment,y} + BE_{s,treatment,y} + BE_{ww,discharge,y} + BE_{s,final,y} \right\}$

Where:

BE_y	=	Baseline emissions in year y (t CO ₂ e)
BE _{power,y}	=	Baseline emissions from electricity or fuel consumption in year y (t CO2e)
$BE_{ww,treatment,y}$	=	Baseline emissions of the wastewater treatment systems affectedby the project activity in year <i>y</i> (t CO ₂ e)
BE _{s,treatment,y}	=	Baseline emissions of the sludge treatment systems affected by the the project activity in year y (t CO2e)
BE _{ww,discharge,y}	=	Baseline methane emissions from degradable organic carbon in treated wastewater discharged into sea/river/lake in yeary (t CO2e). The value of this term is zero for the case 1(b)
BE _{s,final,y}	=	Baseline methane emissions from anaerobic decay of the final sludge produced in year y (t CO ₂ e). If the sludge is controlled combusted, disposed in a landfill with biogas recovery, or used for soil application in the baseline scenario, this term shall be neglected

$BE_{ww,treatment,y} = \sum (Q_{ww,i,y})$	$*COD_{inflow,i,y}$	$*\eta_{COD,BL,i}$	$*MCF_{ww,treatment,BL,i})$	* B _{0,ww} :	$*UF_{BL}$	*GWP _{CH4}
i						

Parameter	Symbol	Unit
Volume of waste water treated	Qww,i,y	m ³ /year
Quanity of ML entering Mother Liquor Treatment Plant		m³/year
COD inlet to WW treatment		kg/year
COD inlet to WW treatment		kg/m3
COD inlet to WW treatment	CODinflow,i,y	t/m³
COD removal efficiency of the baseline treatment system		
i	ηCOD,BL,y	
Methane correction factor for the existing wastewater		
treatment system	MCFww,treatment,BL,i	
		kg CH₄/kg
Methane generation capacity of the wastewater	Bo,ww	COD
Model correction factor	UFBL	
Global warming potential of methane	GWPCH₄	tCO2/tCH₄
Baseline emissions from the baseline waste water		
treatment system	BEww, treatment,y	tCO₂e/year



	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
BEww,										
treatment,y										
tCO₂e/year	11125	12704	14310	14830	13740	13378	11994	14361	14988	15376

Symbol	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
BEthermal,CO2,y										
tCO₂e/year	1438	1739	1068	1329	1171	803	1430	1563	3304	3387

Baseline emissions as per AMS I. C.

$BE_{thermal CO2, y} = (EG_{thermal y} / \eta_{BL, thermal}) * EF_{FF, CO_2}$

Parameter	Symbol	Unit
Total energy generation	EG _{thermal,y}	TJ/year
Efficiency of the boiler	$\eta_{\text{BL,thermal,y}}$	%
Emission factor of FO	EF _{FF,CO2}	tCO₂/TJ
Baseline emissions due to combustion of furnace		
oil	BE _{thermal,CO2,y}	tCO₂e/year

Baseline emissions of the sludge treatment systems affected by the project activity:

As a conservative approach, baseline emissions from the sludge treatment systems have not been considered.

Baseline methane emissions on account of inefficiencies in the baseline wastewater treatment systems and presence of degradable organic carbon in the treated wastewater discharged into river/lake/sea:

Baseline emissions on account of inefficiencies in the baseline wastewater treatment systems and presence of degradable organic carbon in the treated wastewater are not considered as a conservative approach.

Baseline methane emissions from anaerobic decay of the final sludge

As a conservative approach, Methane emissions from anaerobic decay of the final sludge have not been considered in the baseline calculations.



	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
Baseline										
emissions as										
per AMS III H	11125	12704	14310	14830	13740	13378	11994	14361	14988	15376
Baseline										
emissions as										
per AMS I C	1438	1739	1068	1329	1171	803	1430	1563	3304	3387
Total										
Baseline										
Emissions	12563	14443	15378	16159	14911	14181	13424	15924	18292	18763

Project Emissions (PE_y)

Project emissions consists of:

CO2 emissions from electricity and fuel used by the project facilities (PE power,y);

Methane emissions from wastewater treatment systems affected by the project activity, and not equipped with biogas recovery in the project scenario ($PE_{ww,treatment,y}$);

Methane emissions from sludge treatment systems affected by the project activity, and not equipped with biogas recovery in the project situation ($PE_{s,treatment,y}$);

Methane emissions on account of inefficiency of the project activity wastewater treatment systems and presence of degradable organic carbon in treated wastewater (*PE*_{ww,discharge,y});

Methane emissions from the decay of the final sludge generated by the project activity treatment systems ($PE_{s,final,y}$);

Methane fugitive emissions due to inefficiencies in capture systems (PE fugitive, y);Methane emissions

due to incomplete flaring (PE flaring, y);

Methane emissions from biomass stored under anaerobic conditions which would not have occurred in the baseline situation (*PE*_{biomass,y}).



$$PE_{y} = \begin{cases} PE_{power,y} + PE_{ww,treatment,y} + PE_{s,treatment,y} + PE_{ww,discharge,y} + PE_{s,final,y} + \\ PE_{fugitive,y} + PE_{biomass,y} + PE_{flaring,y} \end{cases}$$

Project Emissions as per AMS III.H.

$$PE_{power,y} = \bigcirc EC_{PJ, j, y} * EF_{j,y} * (1 + TDL_{j,y})$$

In case of project activity, CO_2 emissions on account of power used by the project activity are from two different sources, regional electricity grid ($PE_{Grid,y}$) and off grid captive power plant i.e. diesel generator sets ($PE_{DG,y}$).

 $PE_{power,y} = PE_{Grid,y} + PE_{DG,y}$

 $PE_{Grid,y} = EC_{PJ,Grid,y} * EF_{EL,Grid,y} * (1 + TDL_{Grid,y})PE_{DG,y} =$

 $EC_{PJ,DG,y} * EF_{EL,DG,y} * (1 + TDL_{DG,y})$

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
MDy										
tCO₂e/year	19359	17374	12476	14148	12871	8096	12915	15531	27761	26000
PEpower,y										
tCO₂e/year	2155	2218	2122	2188	2124	1951	1705	1918	2125	1789

Methane emissions from wastewater treatment systems affected by the project activity and not equipped with biogas recovery in the project scenario (PE_{ww,treatment,y}),

Project activity will affect existing 4,500 m³/day waste water treatment plant. These emissions shall be calculated as per AMS III.H. Version 19, using an uncertainty factor of 1.12 and data applicable to the project situation ($MCF_{ww,treatment,PJ,k}$ and $\eta PJ,k,y$):

$$PE_{ww,treatment,y} = \sum (Q_{ww,i,y} * COD_{inlow,i,y} * \eta_{PJ,k} * MCF_{ww,treatment,PJ,k}) * B_{o,ww} * UF_{PJ} * GWP_{CH4}$$



Volume of the waste water treated in the year	Qww,i,y	m³/year
Inlet COD to the waste water treatment system	CODinflow,i,y	t/m³
COD removal efficiency of the project treatment system i	ηPJ,k	%
Methane correction factor for project wastewater treatment		
system k	MCFww,teatment,PJ,k	
Methane producing capacity of the wastewater	Bo,ww	kg CH₄/kg COD
Model correction factor to account for model uncertainties	UFPJ	
Global Warming Potential for methane	GWPCH₄	tCO2/tCH₄
Methane emissions from wastewater treatment systems		
affected by the project activity, and not equipped with		
biogas recovery, in year y	PEww,treatment,y	tCO2e/year

$$PE_{ww,discharge,y} = Q_{ww,y} * GWP_{CH4} * B_{o,ww} * UF_{PJ} * COD_{ww,discharge,PJ,y} * MCF_{ww,PJ,discharge}$$

Volume of the waste water treated in the year	Qww,y	m³/year
Chemical oxygen demand of treated wastewater in the		
year	CODww,discharge,PJ,y	t/m³
Methane generation capacity of the wastewater	Bo,ww	kg CH₄/kg COD
Methane correction factor based on type of treatment and		
discharge pathway of the wastewater	MCFww,PJ,discharge	
Model Correction factor to account for model		
uncertainities	UF _{PJ}	
Global warming potential of methane	GWPCH₄	tCO2/tCH₄
Methane emissions on account of inefficiency of the		
project activity wastewater treatment systems and		
presence of degradable organic carbon in treated		
wastewater	PEww,discharge,y	tCO2e/year



Methane emissions from sludge treatment systems affected by the project activity, andnot equipped with biogas recovery in the project situation (PEs,treatment)

These project emissions are not considered as sludge treatment systems are not affected by the project activity.

Methane emissions from degradable organic carbon in treated wastewater inyear y (PE,ww, discharge,y)

These emissions shall be calculated as per AMS III.H using an uncertainty factor of 1.12 and data applicable to the project situation (COD_{ww,discharge,PJ,y} MCF_{ww},PJ,discharge)

Methane emissions from the decay of the final sludge generated by the project activity treatment systems ($PE_{s,final,y}$)

As explained above, if the sludge is controlled combusted, disposed in a landfill with biogas recovery, or used for soil application in aerobic conditions in the project activity, this term shall be neglected. Since the sludge generated in the project activity would be used for soil application, methane emissions from the decay of the sludge are neglected.

Methane fugitive emissions on account of inefficiencies in capture systems (PE_{fugitive,y})

As per AMS III. H. version 19, project activity emissions form methane release in capture systems are determined as follows,

$$PE_{fugitive,y} = PE_{fugitive,ww,y} + PE_{fugitive,s,y}$$

$$PE_{fugitive_{s,y}} = 0$$

$$PE_{fugitive,ww,y} = (1 - CFE_{ww}) * MEP_{ww,treatment,y} * GWP_{CH4}$$

Capture efficiency of the biogas recovery equipment in the		
wastewater treatment systems	CFEww	
Methane emission potential of wastewater treatment		
systems equipped with		
biogas recovery system in year y	MEPww,treatment,y	t
Volume of the ML treated in the year	Qww,y	m³/year
		kg CH₄/kg
methane generation capacity of the wastewater	Bo,ww	COD
Model Correction factor to account for model uncertainities	UFPJ	
Global Warming Potential for methane	GWPCH ₄	tCO₂/tCH₄



Chemical oxygen demand removed by the treatment system		
k (45 m3 Mother Liquor Treatment Plant) of the project		
activity equipped with biogas recovery equipment in year y	CODremoved,PJ,k,y	t/m ³
Methane correction factor for the project wastewater		
treatment systems k equipped with biogas recovery		
equipment	MCFww,treatment,PJ,y	
Methane fugitive emissions on account of inefficiencies in		
capture systems in MLTP	PEfugitive,ww,y	tCO2e/year
For Waste Water Treatment Plant (WWTP):		
Capture efficiency of the biogas recovery equipment in the		
wastewater treatment systems	CFEww	
Methane emission potential of wastewater treatment		
systems equipped with		
biogas recovery system in year y	MEPww,treatment,y	t
Volume of the waste water treated in the year	Qww,y	m³/year
		kg CH₄/kg
Methane generation capacity of the wastewater	Bo,ww	COD
Model Correction factor to account for model uncertainities	UFPJ	
Global Warming Potential for methane	GWPCH4	tCO2/tCH₄
Chemical oxygen demand removed by the treatment system		
k (120 m3 Mother Liquor Treatment Plant) of the project		
activity equipped with biogas recovery equipment in year y	CODremoved,PJ,k,y	t/m3
Methane correction factor for the project wastewater		
treatment systems k equipped with biogas recovery		
equipment	MCFww,treatment,PJ,y	
Methane fugitive emissions on account of inefficiencies in		
capture systems in WWTP	PEfugitive,ww,y	tCO2e/year
Methane fugitive emissions on account of inefficiencies in		
capture systems	PEfugitive,y	tCO2e/year

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
PEww,treatment,y										
tCO2e/year	0	0	0	0	0	0	0	0	0	0
PEww,discharge,y										
tCO2e/year	47	55	64	73	80	67	62	76	77	76
PEfugitive,y										
tCO2e/year	112	132	122	111	84	70	63	82	89	81

Methane emissions due to incomplete flaring in year y ($PE_{flaring,y}$)

In the project activity, generated biogas will be consumed in the heat generating



equipment's (boilers). The project activity involves one heat generating equipment's (6TPH (F&A 100^oC) i.e. RFB-60 Boiler. When this boiler is forced shut down or is under maintenance, biogas can be supplied to another boilers (SM140.1 & SM140.2). It very unlikely that both the heat generating equipment's are under maintenance or forced shut down.

However, if such condition occurs, the number of hours of operation of flare shall be monitored as H_{flare} and the quantity of biogas flared shall be obtained by multiplying the flare capacity and number of hours of operation of flare. The project activity involves open flaring system. This system is now not operational in and use of the same is very unlikely because the generated biogas will be used in the boilers. Hence, the default value to be adapted for flare efficiency is 0%.

Leakage (LE_{WW, y}):

There is no transfer of equipment from another activity nor the existing equipment is transferred to another activity, hence there is no leakage has been considered for this project activity.

For Computation of Emission reductions based on ex post values for mother liquor treatment (under AMS III.H), conservative values shall be considered as per:

 $\begin{aligned} ER_{y,ex\ post} &= \min((BE_{y,ex\ post} - PE_{y,ex\ post} - LE_{y,ex\ post}),\\ (MD_y - PE_{power,y} - PE_{biomass,y} - LE_{y,ex\ post}))\end{aligned}$

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
Total Project										
emissions as										
per AMS III.H.	2314	2405	2308	2372	2288	2088	1830	2076	2291	1946

Project Emissions as per AMS I. C.

CO₂ emission from onsite consumption of fossil fuels due to the project activity

$$PE_{FC,boiler,y} = \left(\sum_{FO} FC_{FO,bolier,y} \times COEF_{FO,y}\right)$$

Quantity of Fossil fuel used in the project activity	FCFO,boiler,y	kg/year
Coefficient of emission factor	COEFFO,y	



NCV of FO	NCVFO,y	TJ/kg
Emission factor of FO	EFCO2,FO,y	tCO₂/TJ
CO2 emissions from on-site consumption of fossil fuels due		
to the project activity in year y	PEFC,boiler,y	tCO ₂ /year
Total Project emissions as per AMS I.C.		tCO₂e/year

'CO₂ emissions from electricity consumption by the project activity' will be considered and calculated as per AMS III.H. version 19 and are described above under $PE_{ww,y}$.

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
Total Project										
emissions as										
per AMS I.C.	195	49	41	0	0	47	0	0	0	0

Total project emissions:

Therefore, Project emissions due to thermal energygeneration will be, PE_{thermal,y} = PE_{FC,boiler,y}

Leakage $(LE_{thermal,y})$:

Leakage emissions are not considered since there is no transfer of equipment from another activity.

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023
Total Project emissions as										
per AMS III.H.	2314	2405	2308	2372	2288	2088	1830	2076	2291	1946
Total Project emissions as										
per AMS I.C.	195	49	41	0	0	47	0	0	0	0
Total Project										
Emissions	2509	2454	2349	2372	2288	2135	1830	2076	2291	1946

Establishment and description of baseline scenario (UNFCCC CDM-UCR Protocol)

The baseline scenario of the project activity is identified as:

The baseline of the project activity is identified as per paragraph 21, 22, 24, 25 & 26 of AMS III.H ver. 19. As per paragraph 24 AMS III. H ver.19, "Wastewater and sludge treatment systems equipped with a biogas recovery facility in the baseline shall be excluded from the baseline emission calculations." the existing WWTP is excluded from the baseline emission calculations.



Mother Liquor was treated in anaerobic lagoons which was not equipped with biogas recovery and hence, baseline emissions for the systems affected by the project activity are considered. The applicable Methane equipped Correction Factor (MCF) will be determined based on the given table AMS III.H.2.

And baseline of the project activity is identified as per paragraph 63 of AMS I.C. Version 22 as, for project activities that seek to retrofit or modify an existing facility for the purpose of fuel switch from fossil fuels to biomass in heat generation equipment, the baseline emissions shall be calculated as per equation 2". The equation 3 refers to paragraph 34 of the methodology. Thus, paragraph 34 is identified as baseline scenario.

The project activity involves mother liquor treatment in anaerobic digesters that otherwise would continue to be treated in anaerobic deep lagoons without any biogas recovery. Generated biogas in the project activity shall be used in the boiler thereby replacing corresponding quantity of FO.

Hence, simplified baseline for the project activity is, continued treatment of Mother Liquor in anaerobic deep lagoons without biogas recovery and consumption of equivalent quantity of FO that otherwise would have been consumed in the boiler to generate corresponding quantity of steam.

Emission Reductions (ER_y):

Therefore, total emission reduction because of this project activity is,

$$ER_{y} = ER_{ww,y} + ER_{thermal,y}$$

	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023		
ERww,y	8811	10299	10354	11960	10747	6145	10164	12285	12697	13430		
ERthermal,y	1243	1690	1027	1329	1171	756	1430	1563	3304	3387		
	10054	11989	11381	13289	11918	6901	11594	13848	16001	16817		
ERy	1,23,792											

Total Emission Reductions (ER_y) = 1,23,792 CoUs (1,23,792 tCO₂eq)



Conclusions:

Based on the audit conducted on the basis of UCR Protocol, which draws reference from UCR Standard, CDM UNFCCC Methodology AMS III. H: Methodology for methane recovery in wastewater treatment. version 19 and AMS-I.C: Methodology for Thermal energy production with or without electricity version 22, the audit conducted onsite and the documents verified and submitted during the verification including the Data, Project Concept Note (PCN) / Monitoring Report (MR), SQAC is able to certify that the emission reductions from the project - Wastewater Treatment and Biogas Recovery Project, SDDPL, Baramati, Maharashtra, India, (UCR ID – 421) for the period **01/01/2014 to 31/12/2023** amounts to **1,23,792 tCO₂ (1,23,792 COUs)**



Santosh Nair Lead Verifier (Signature)



Sheetal Wader Verifier (Signature)

Praful Shinganapurkar Senior Internal Reviewer (Signature)

Date: 10/04/2024